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Tensile strength of thin-ply quasi-isotropic laminates: is it controlled by fiber failure or by other mechanisms?

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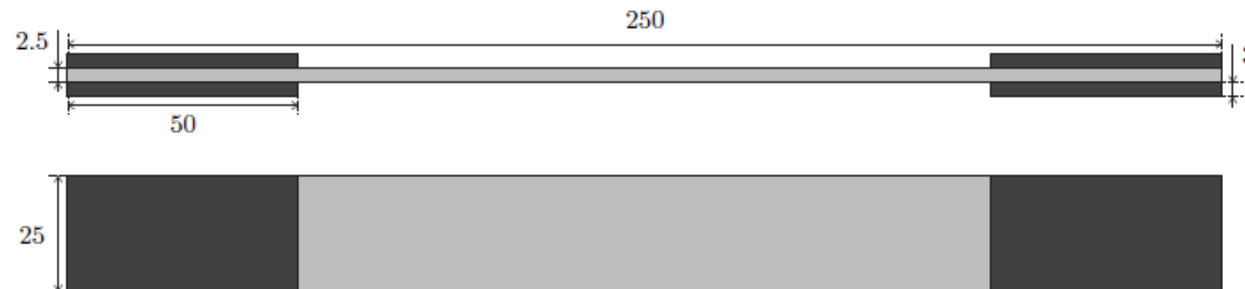
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27.03.2023

Context

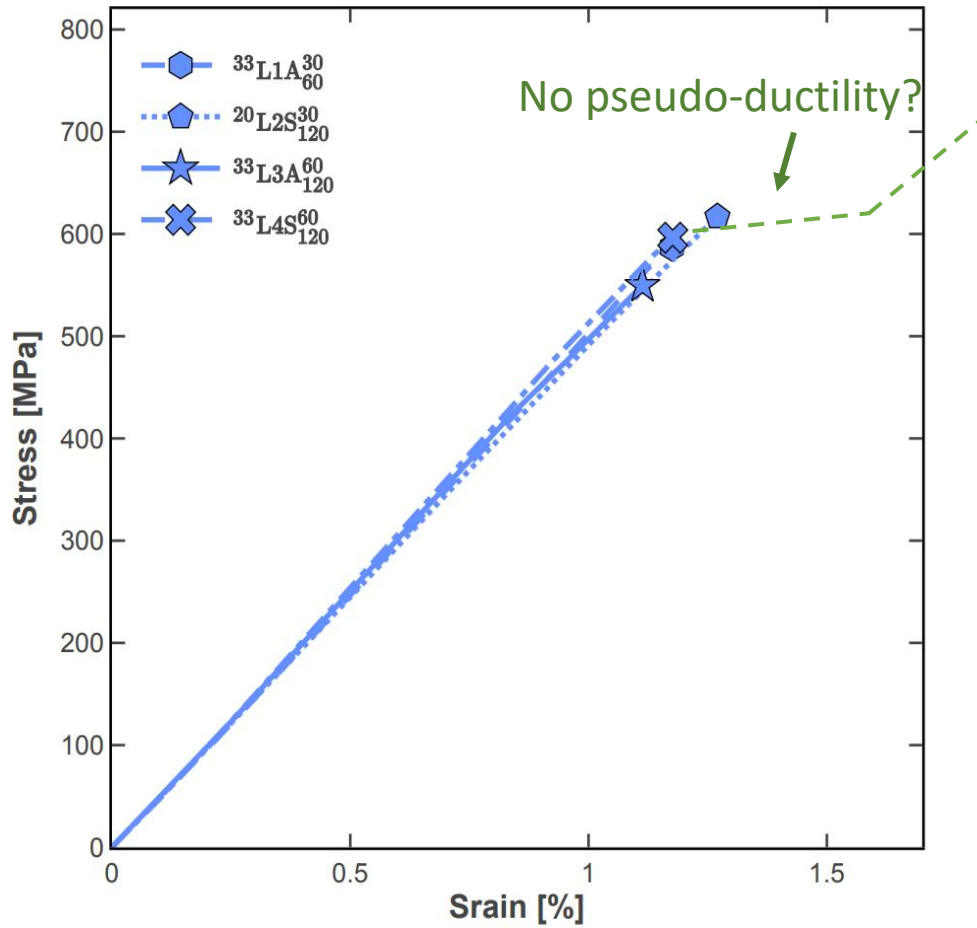
- **PhD Thesis of Guillaume Broggi EPFL** on Hybrid thin ply composites
 - Low strain / high modulus fibre HR40: $E = 375 \text{ GPa} / \epsilon_{\text{ult}} = 1.1\%$
 - High strain / low modulus fibre 34-700: $E = 234 \text{ GPa} / \epsilon_{\text{ult}} = 2.0\%$
 - Resin NTPT TP415, 135°C curing, rubber toughened
 - Prepreg: UD, ply fibre areal weight = 60 g/m² for 34-700; 29 g/m² for HR40; 37% resin weight
- Design of pseudo ductile laminates based on those hypotheses
- Unnotched tensile test specimens based on ASTM D3039 with glued aluminium tabs, layup $[45/90/-45/0]_{\text{ns}}$
- Several hybrids layups + baseline HR40 @29g/m² and 34-700 @60, 120 & 180 g/m²
- Acoustic emission monitoring for detection of onset of damage + strain gage for strain measurement



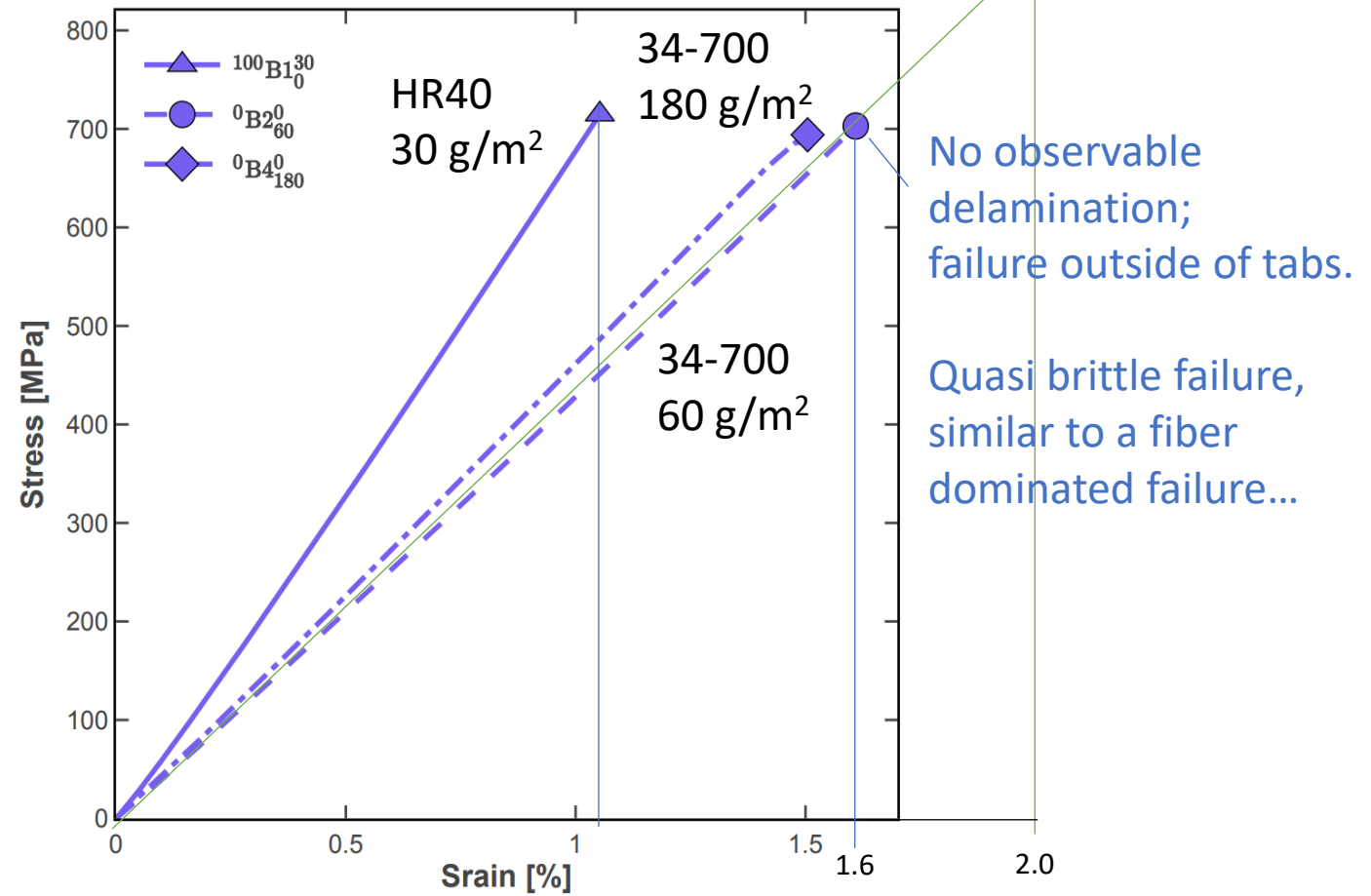
UD QISO tensile test results

Interlayer hybrids

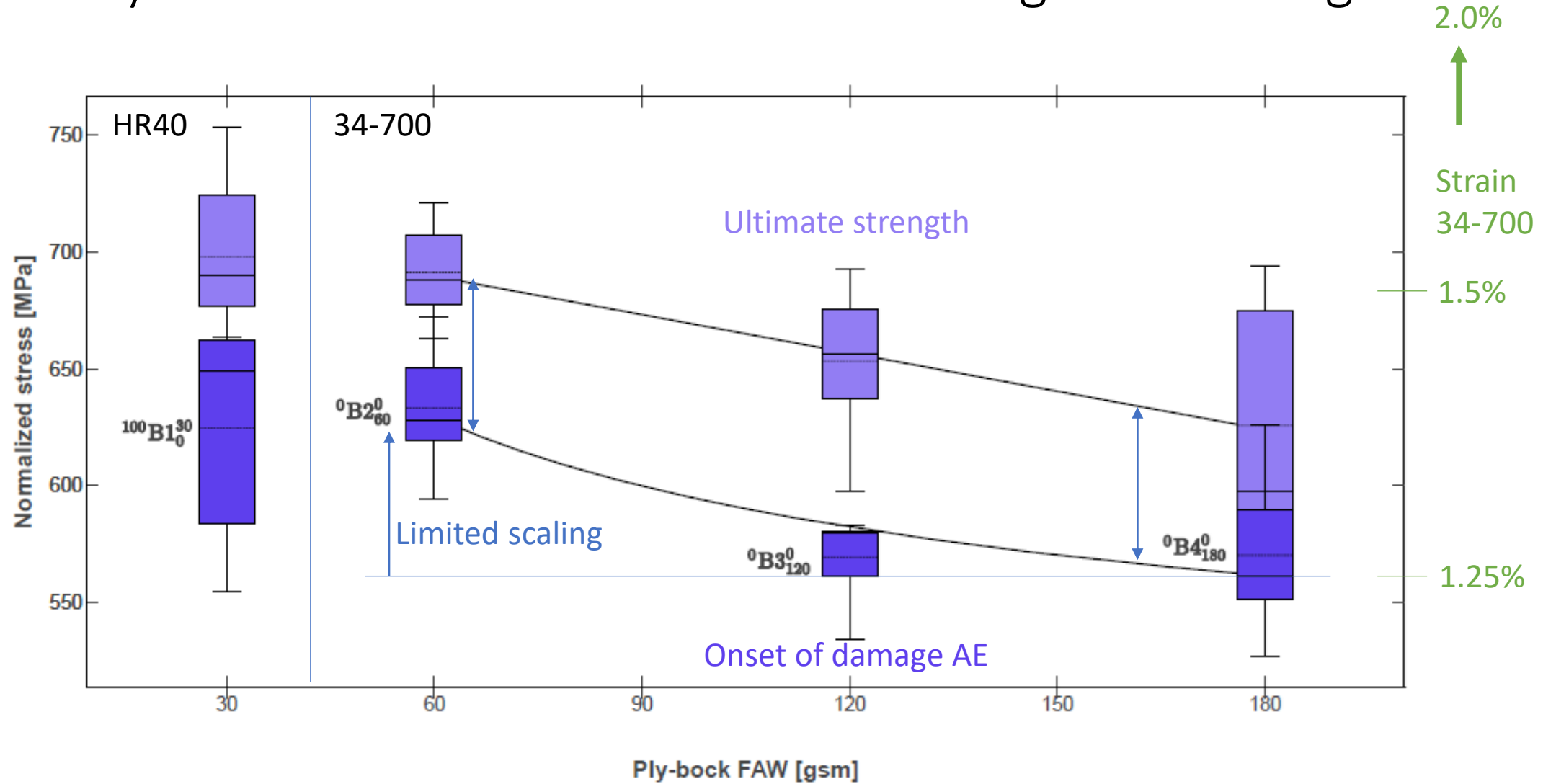
Resin: TP415



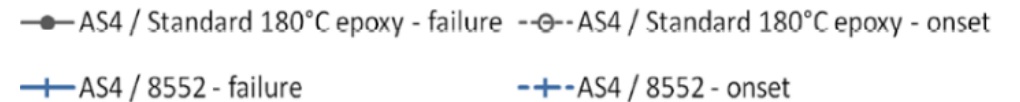
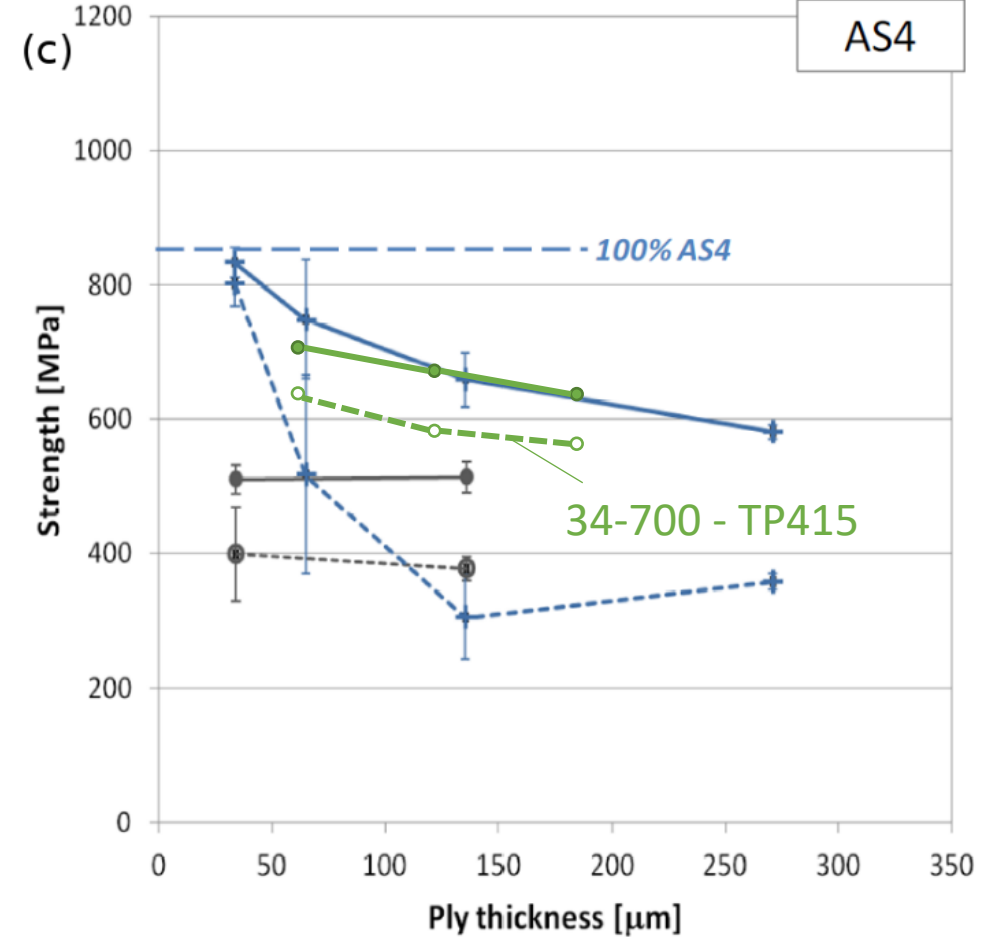
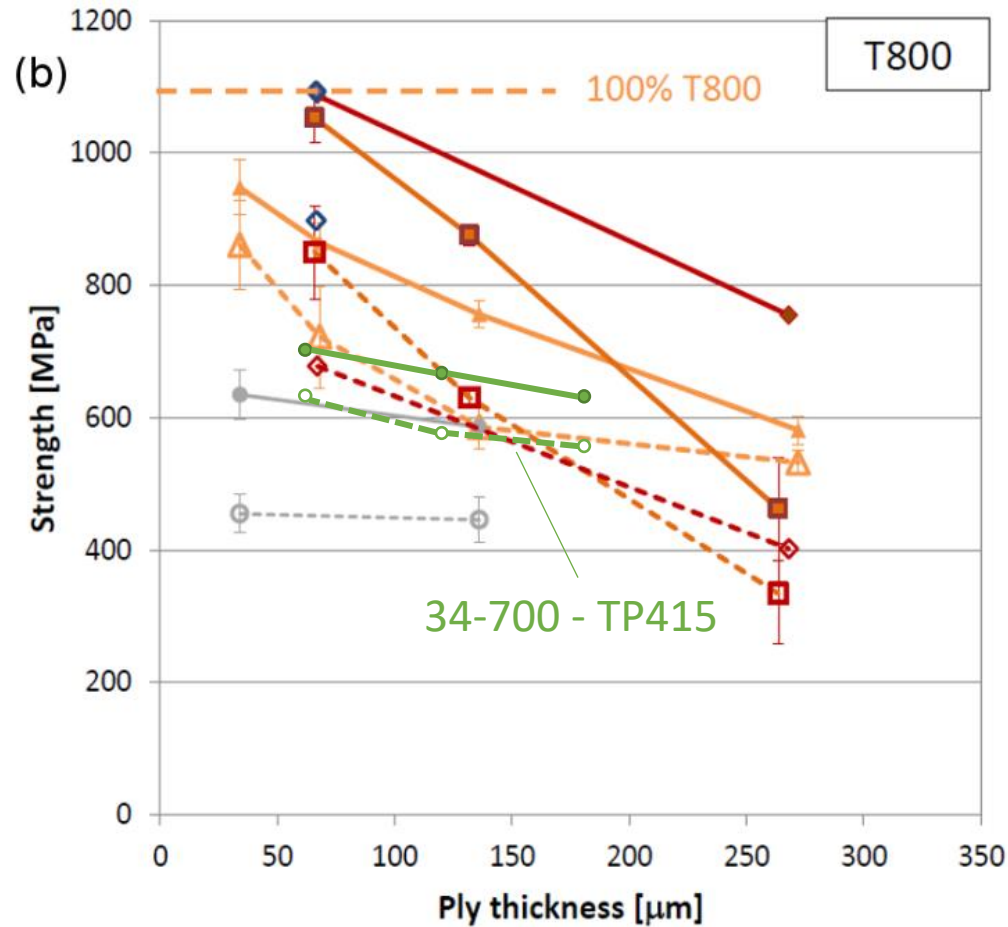
Baselines



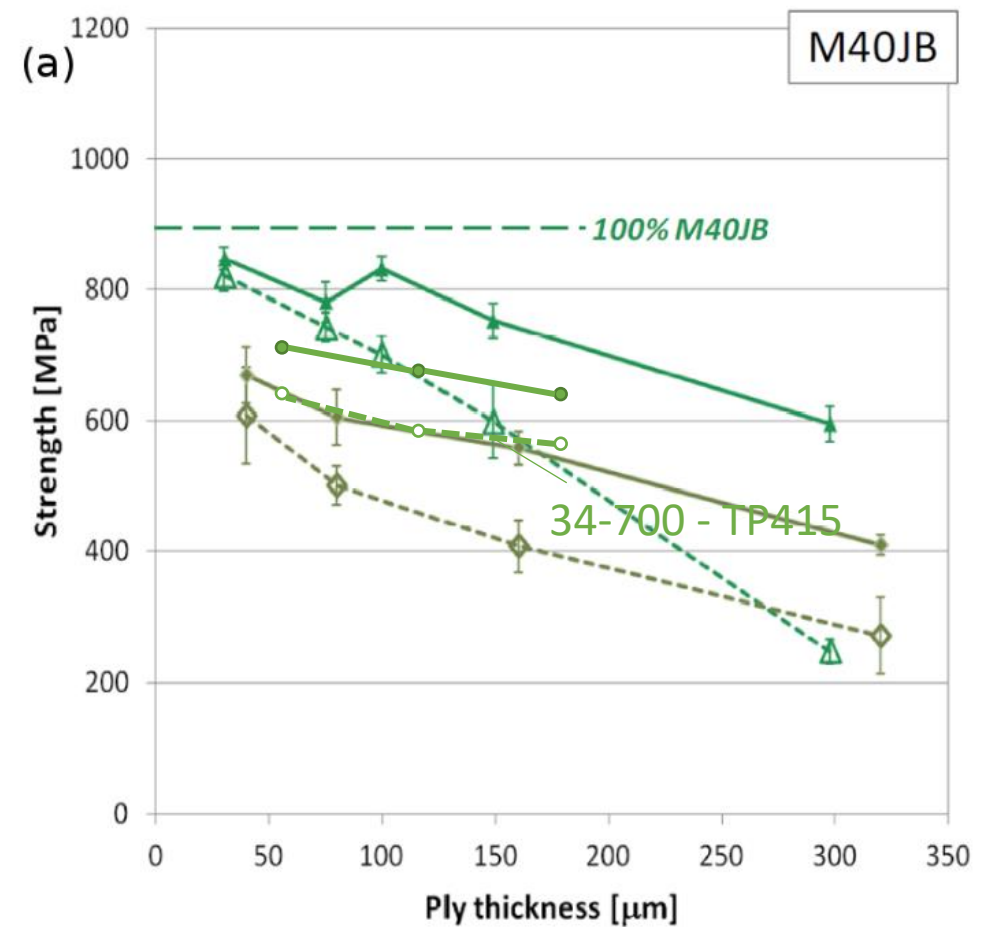
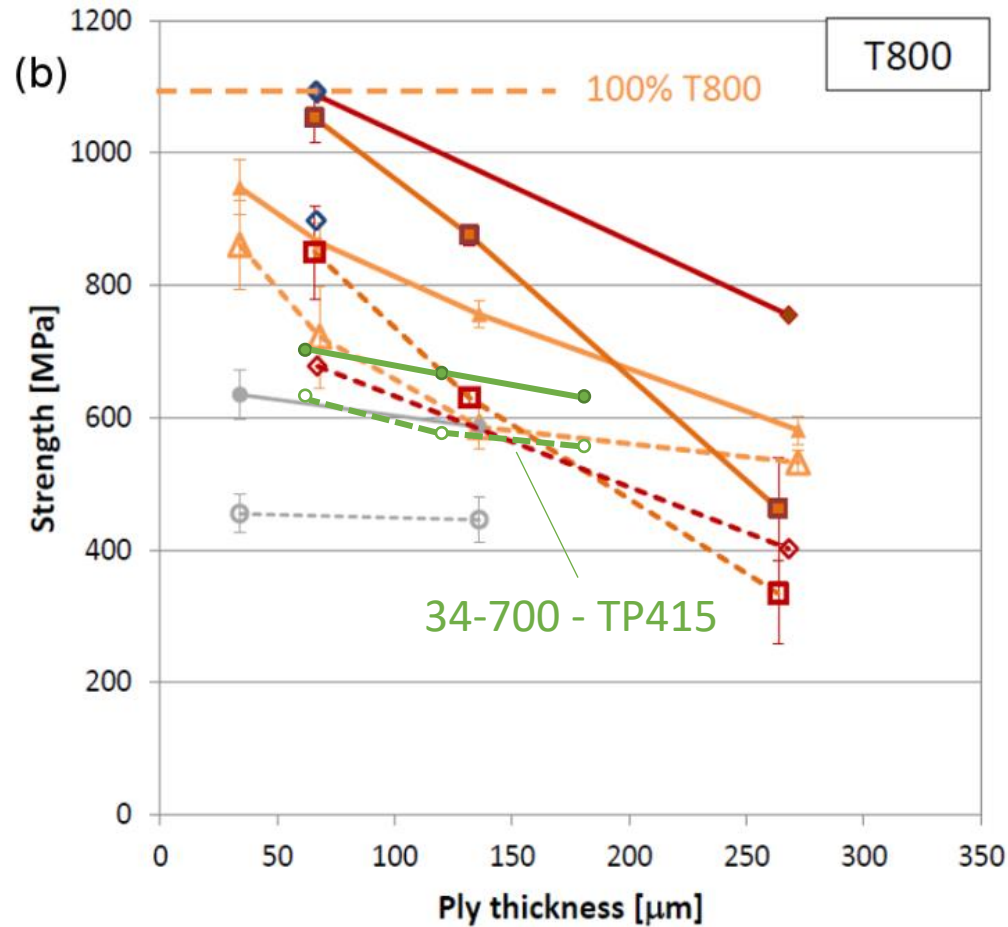
Ply thickness effects on onset of damage and strength



Comparison with other systems



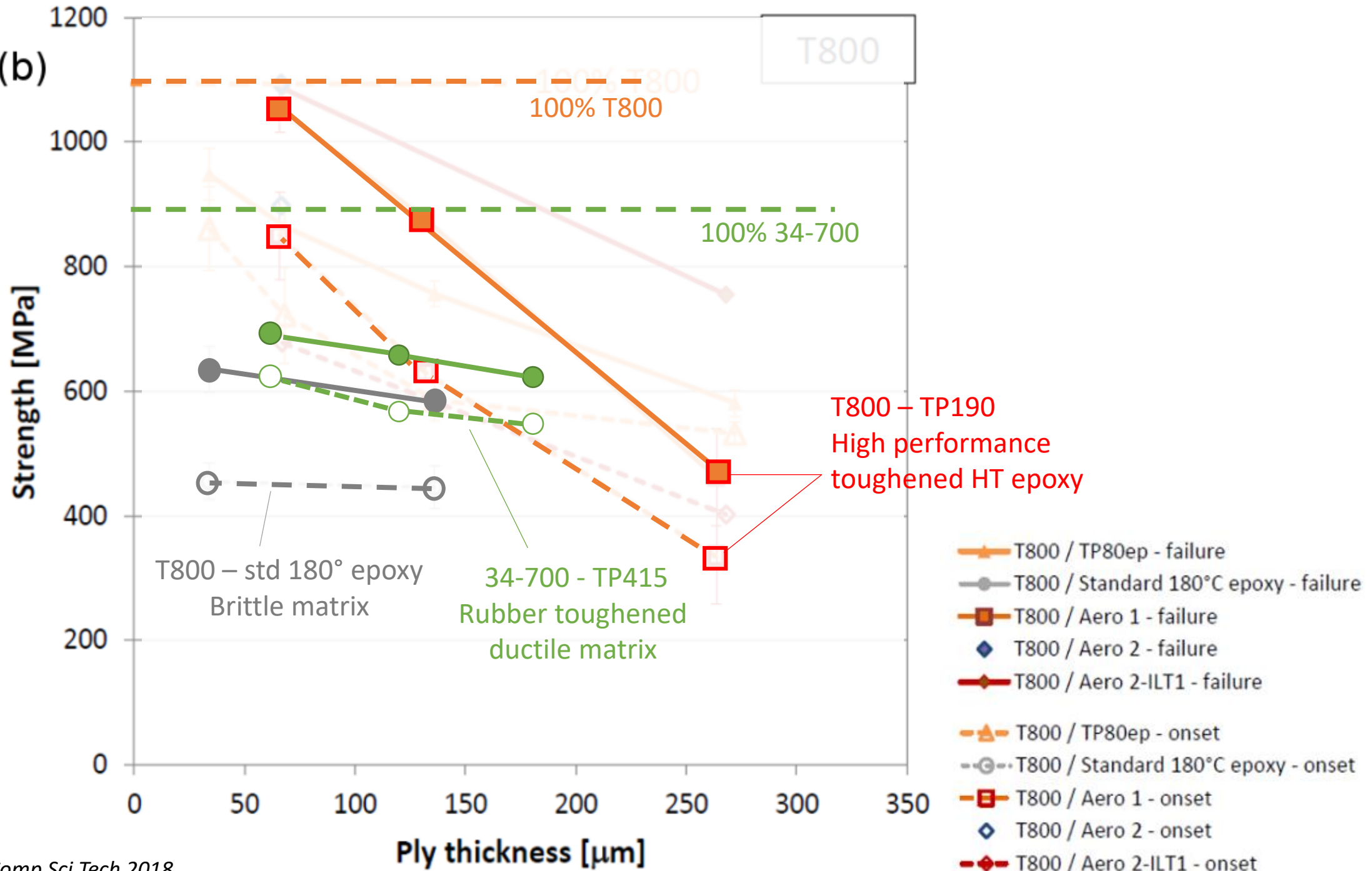
Comparison with other systems



- ▲— T800 / TP80ep - failure
- T800 / Standard 180°C epoxy - failure
- T800 / Aero 1 - failure
- ◆— T800 / Aero 2 - failure
- ◆— T800 / Aero 2-ILT1 - failure
- ▲— T800 / TP80ep - onset
- T800 / Standard 180°C epoxy - onset
- T800 / Aero 1 - onset
- ◆— T800 / Aero 2 - onset
- ◆— T800 / Aero 2-ILT1 - onset

- ▲— M40JB / TP80ep - failure
- ◆— M40JB / TP120ep - failure
- ▲— M40JB / TP80ep - onset
- ◇— M40JB / TP120ep - onset

(b)



Effect of matrix on very thin-ply QISO UNT

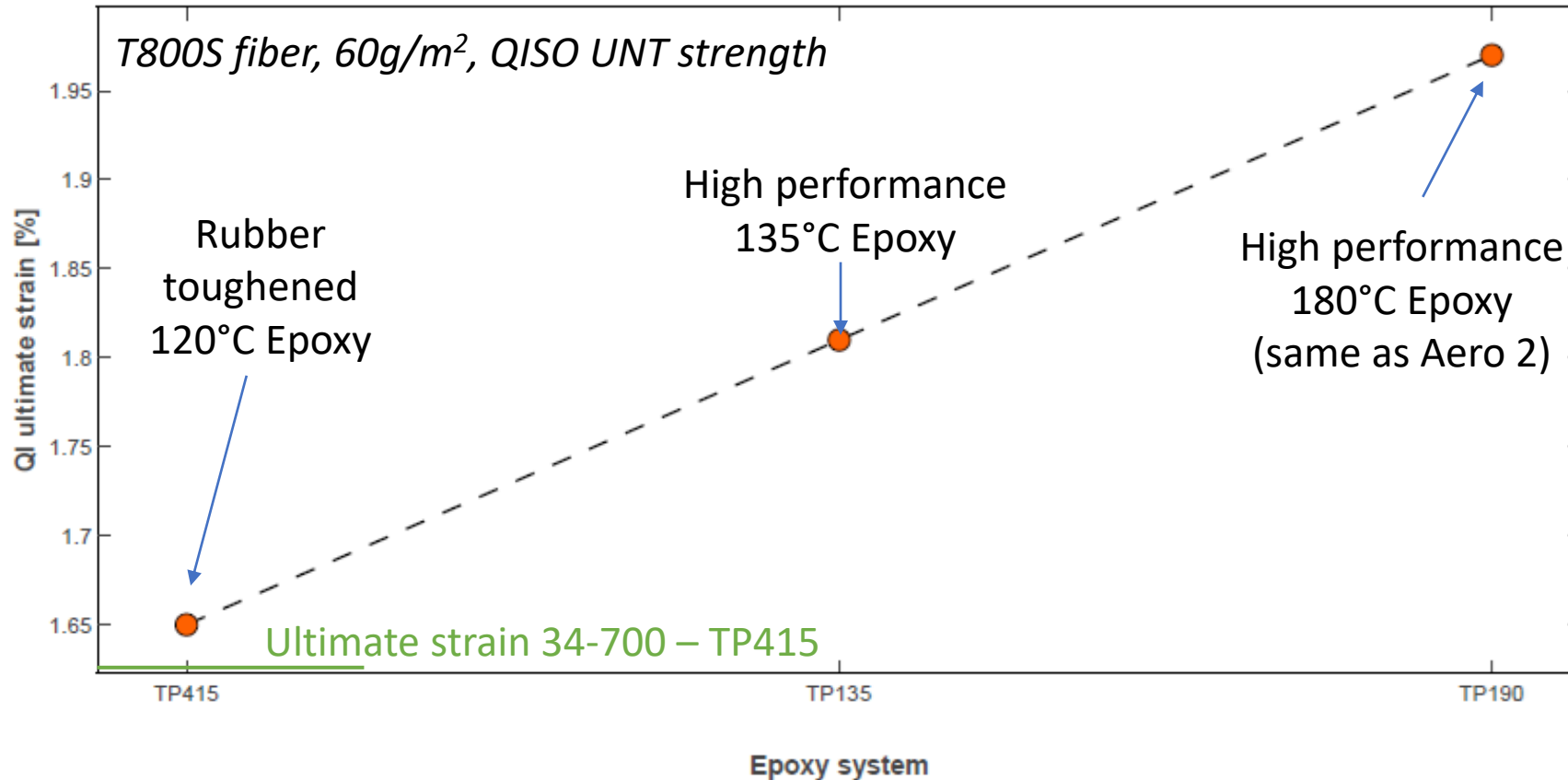
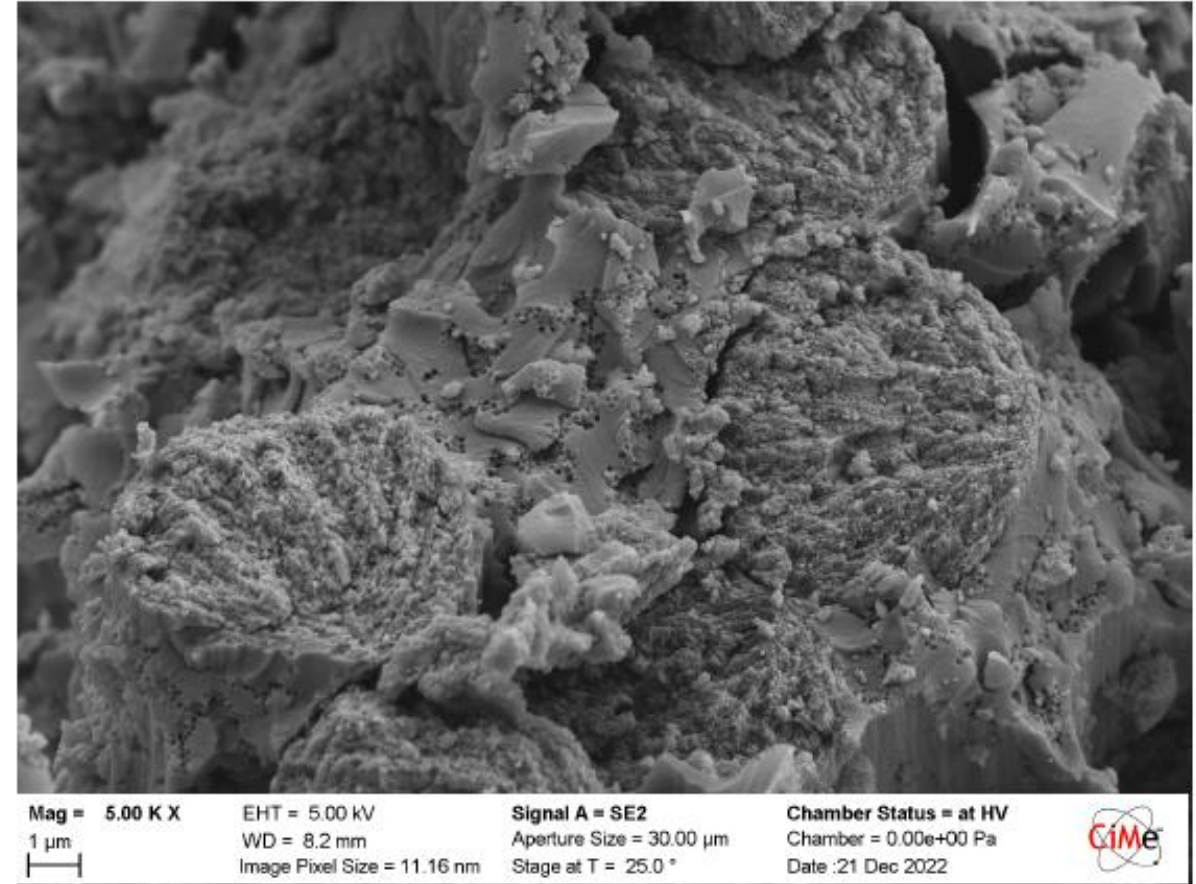
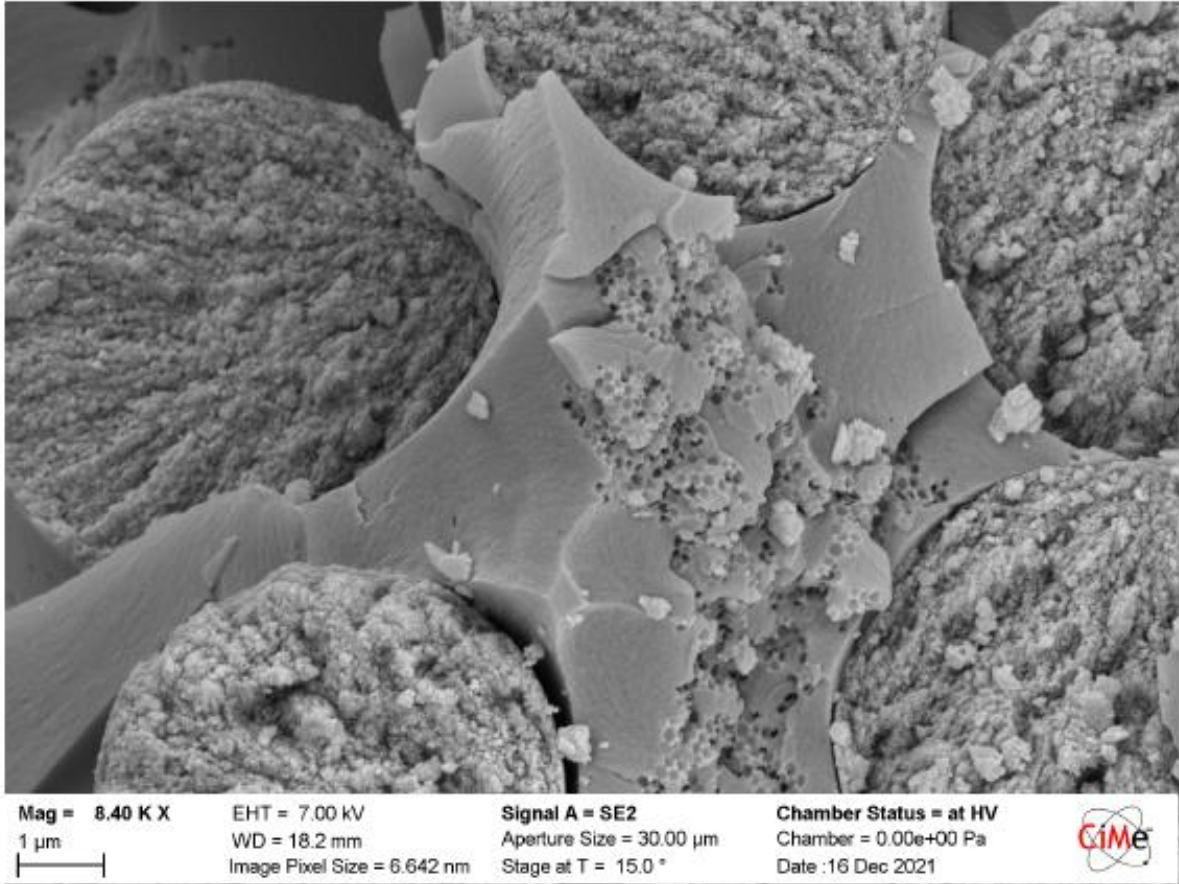


Figure 7.31: QI ultimate strain achieved with T800S carbon fibers and a plt FAW of $60 \text{ g} \cdot \text{m}^{-2}$ for NTPT epoxy systems TP415, TP315 and TP190, according to their datasheet. An higher ultimate strain indicates a better thin-ply effect. For reference, the T800S ultimate strain reported by its datasheet is 2%.

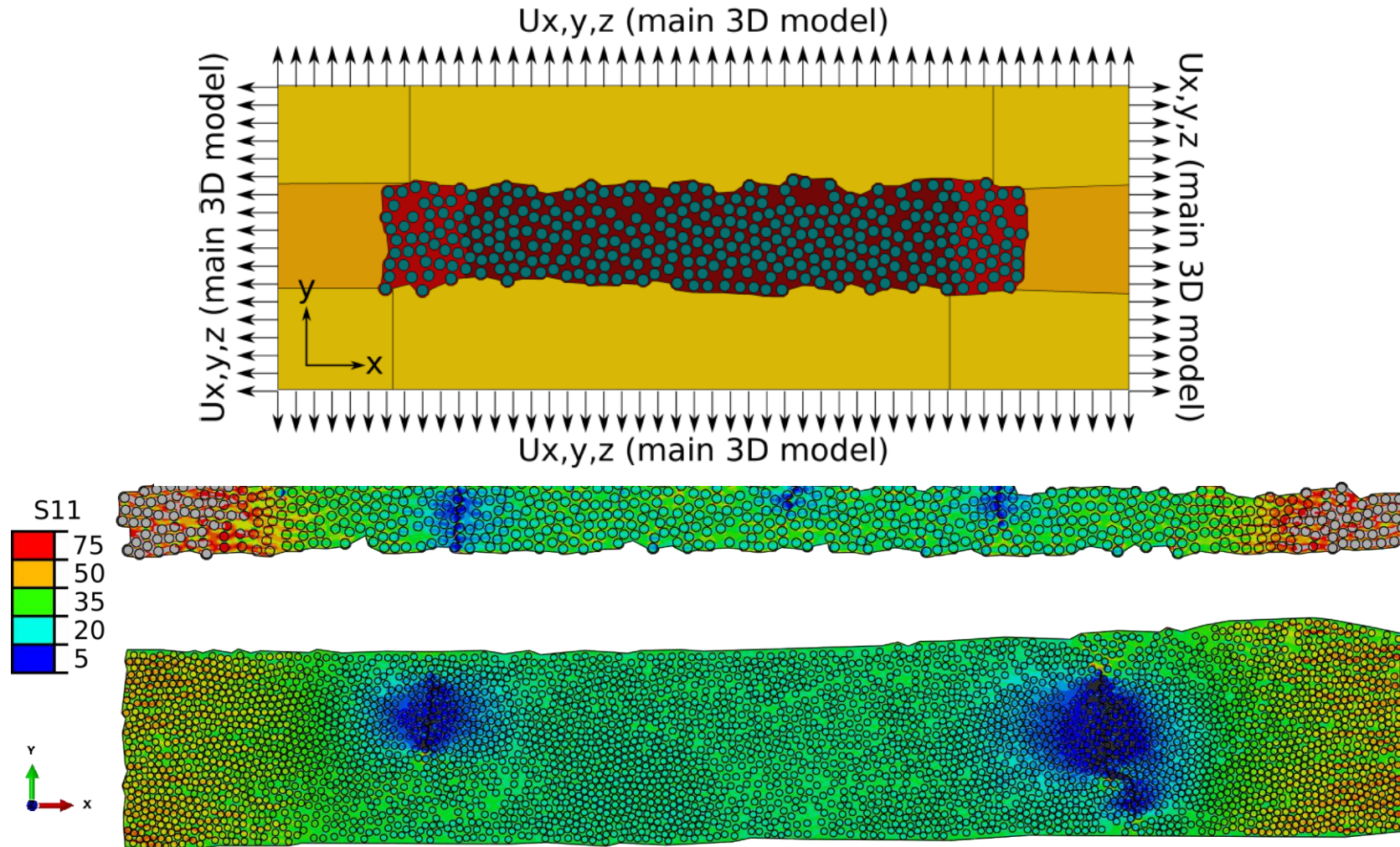
Src : <https://www.thinplytechnology.com/datasheets>

Fracture surface investigation SEM



Rubber Toughener = Void nucleation sites in the matrix?

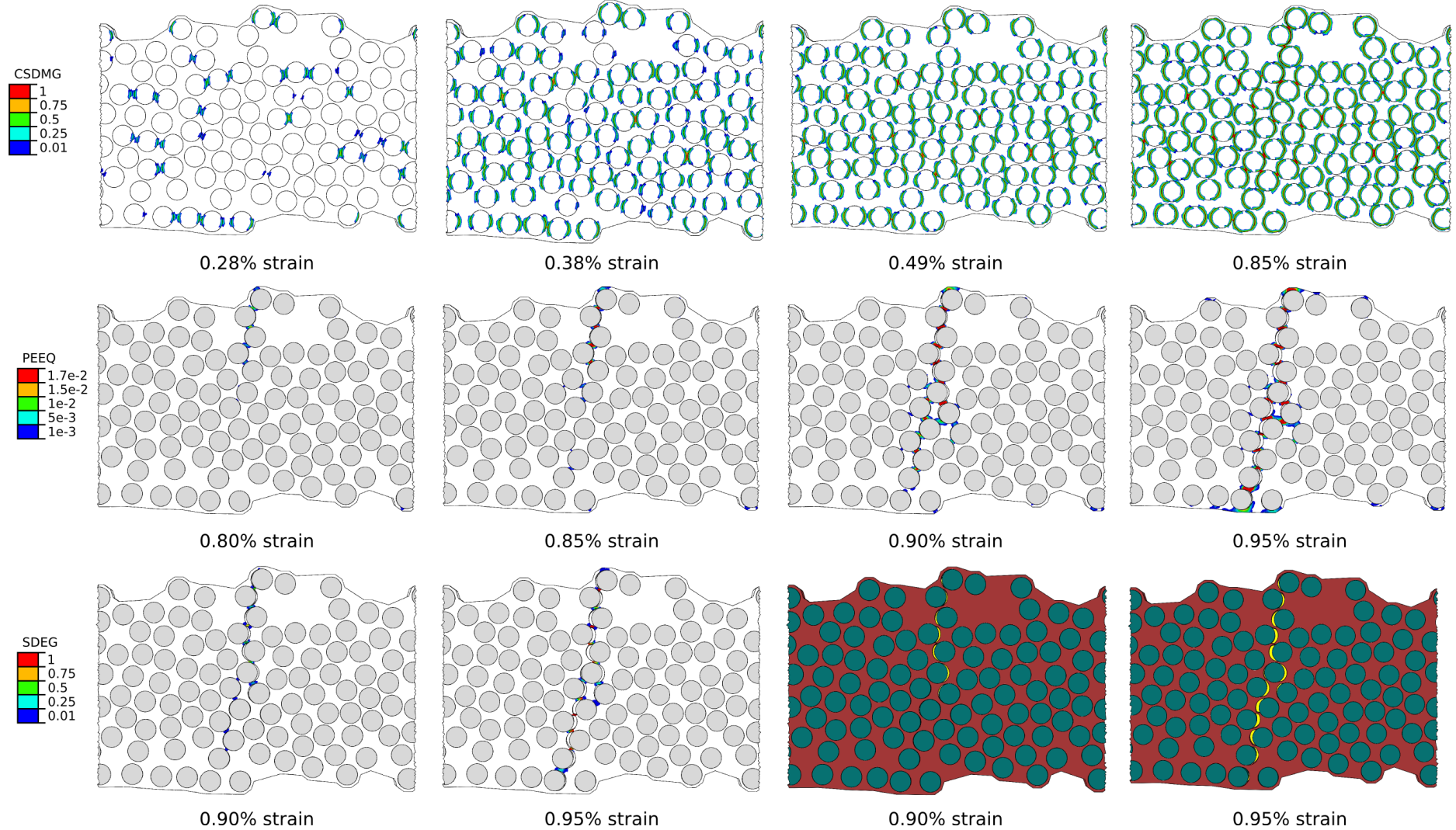
Effect of matrix on very thin-ply QISO UNT



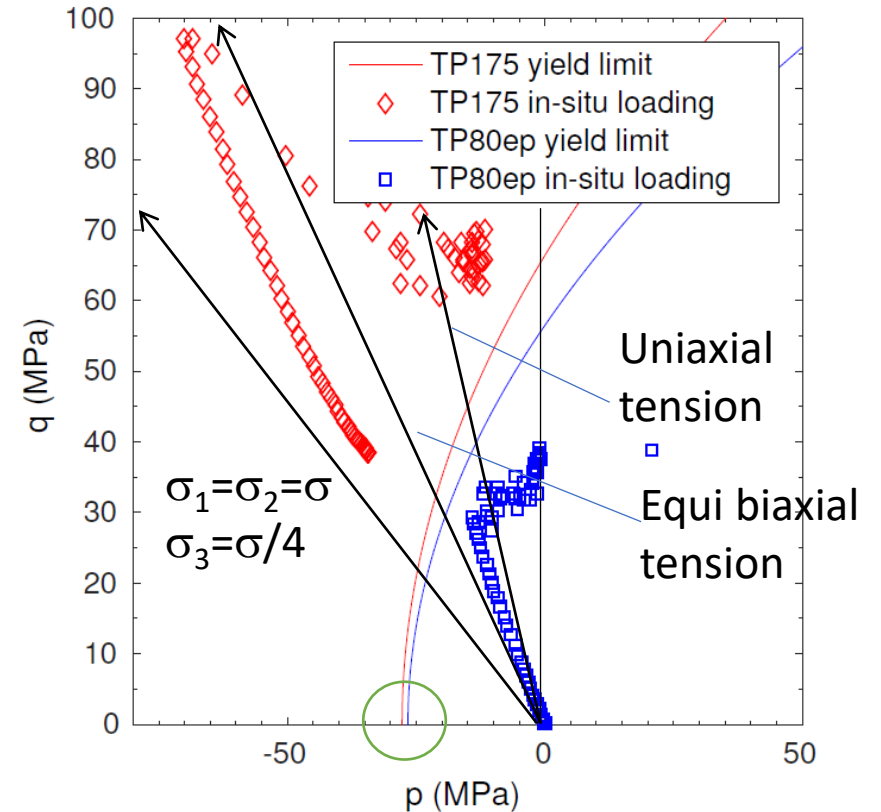
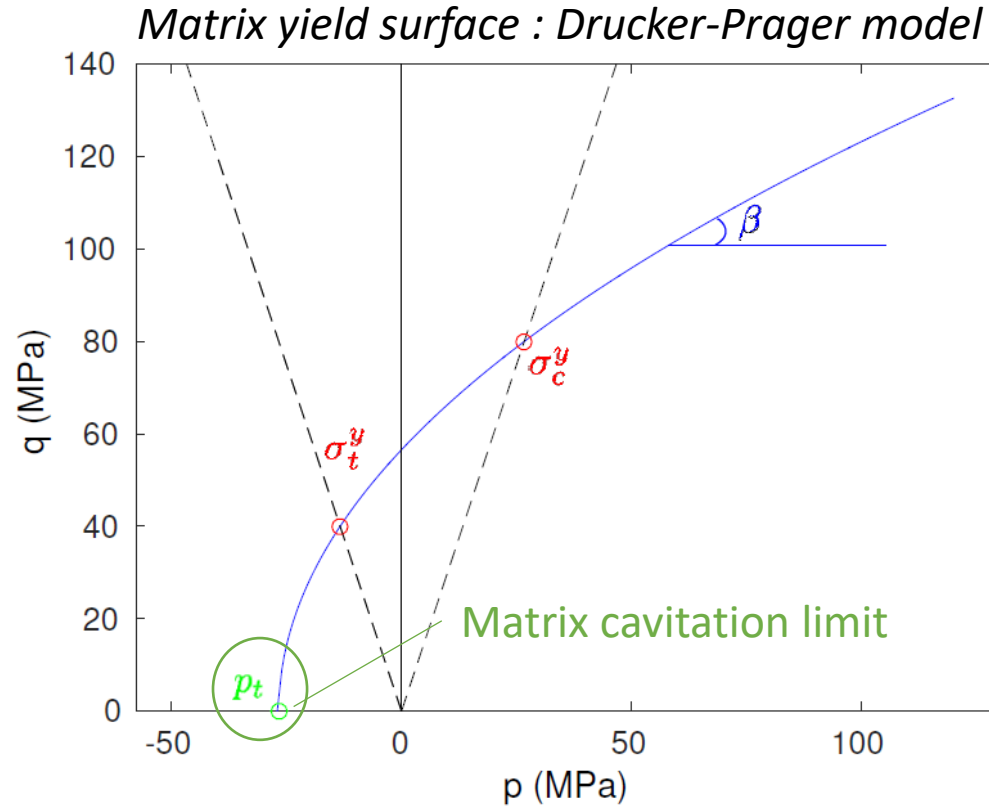
Src : PhD Thesis S. Kohler, EPFL, 2019, <https://infoscience.epfl.ch/record/263781?ln=fr>

S. Kohler et al., Composites Part A, 2019, <https://doi.org/10.1016/j.compositesa.2019.05.036>

Effect of matrix on very thin-ply QISO UNT



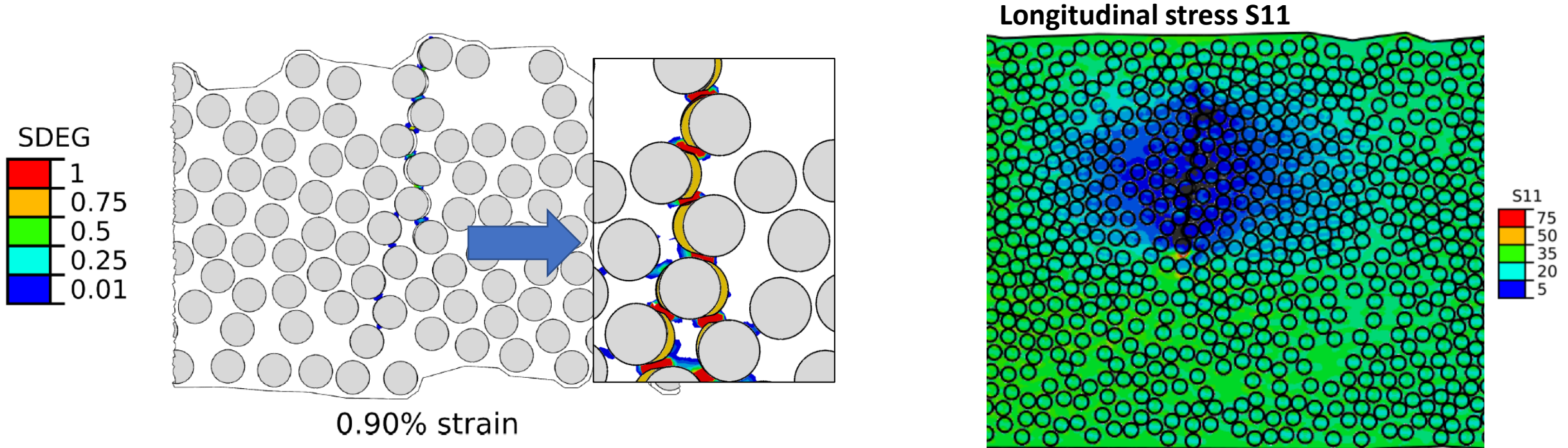
Effect of matrix on very thin-ply QISO UNT



(a) Matrix P-Q graph

FIGURE 6: Identified Drucker-Prager model, with the experimentally measured uniaxial results shown in red and the deduced hydrostatic strength shown in green. p is the hydrostatic pressure and q the equivalent von Mises stress

Effect of matrix on very thin-ply QISO UNT



High triaxial stresses between closely packed fibers : potential site for void nucleation and early transverse fracture



Conclusion

- With optimized resins, possible to reach a ultimate strain in quasi isotropic UNT of ~98% of the fiber with (very) thin-ply composites
- Other resin systems show early transverse cracking due to:
 - Resin brittleness: resin need to be able to sustain at least 2x the ultimate strain of the fiber under biaxial loading
 - Possible early cavitation due to weak inclusions / additives or weak toughener
- In the case of the TP415 -34-700 system, the fracture looked like a brittle fracture of the 0° ply without sign of early transverse cracking or delamination
- The resin can affect the ultimate strength of even very thin ply quasi isotropic composites
- Optimal resin for thick plies = high toughness to prevent cracking; for thinner plies = high cavitation limit , fiber adhesion and ductility

THANK YOU FOR YOUR ATTENTION

This research was supported by :



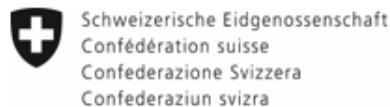
EU Horizon 2020 , Marie Skłodowska-Curie grant agreement No 765881



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Swiss National Science Foundation ,
SNF grant 200021_156207



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